

Optimization studies of Adsorptive Tendency of Flamboyant Pod Bark in Wastewater Treatment of 2,4,6-Trichlorophenol using Response Surface Methodology.

Abstract

Adsorptive capacity of an adsorbent is the main parameter used to categorise efficiency of an adsorbent regardless of its source and a parametric study into the influence of variables that influence adsorptive capacity will enhance the performance of an adsorbent. The experiments used for this study were designed towards the determination of adsorption capacity of flamboyant pod bark activated carbon (FPBAC) as a function of agitation rate, contact time, adsorbent dosage and initial concentration using Central Composite Design (CCD) in Response Surface Methodology (RSM). The result show that the developed adsorptive capacity model was suitable for prediction with a correlation coefficient of 0.9985 without further adjustment to the experimental data and nine out of the twelve variables in the model developed are significant model terms. The maximum adsorption capacity of 34.33 was achieved when agitation rate, contact time, adsorbent dosage and initial concentration were fixed at 151.88 rpm, 120 sec, 0.15 g and 200 mg/g at a desirability of 0.893.

Keywords: Flamboyant Pod Bark, Optimization, Adsorption, Wastewater, Trichlorophenol.

Introduction

Water is one of the most essential components for the existence of life (Bansode *et al.*, 2004) and water quality plays a major role in a measure of wildlife and human health (Baseri *et al.*, 2013). The increase in demand for safe and clean water which either comes from the freshwater or reusing of wastewater directly or indirectly was related to world population increase. Wastewater refers to water that has been adversely affected in quality as a result of human or industrial activities which make it unsafe for usage in its current form (Bansode *et al.*, 2004). Wastewater contains a complex mixture of solids and dissolved components. The dissolve components are present in very small concentrations and composes of organic compounds (persistent organic pollutant, surfactants and oils), inorganic compounds (heavy metals and soluble ions), suspended solids and gases such as oxygen and hydrogen sulphide (Amuda and Ibrahim, 2006). The continuous discharge of organic pollutants which are not degradable from effluents of manufacturing industries into water bodies has become a threat to the global community and thus poses a serious threat to the survival of life (Igwe *et al.*, 2003). Some of the health challenges related to persistent organic pollutant in the environment are dizziness, chest pain, tightness of chest, dry cough, shortness of breath, rapid respiration, nephritis and extreme (Hameed *et al.*, 2009).

Phenol and its derivatives are one of the undesirable components in effluents of industrial wastewater such as agro-chemical, textile, paint, pulp and paper industries. These compounds are toxic and exhibited the characteristics of a weak acid (Hameed *et al.*, 2009). It can easily permeate into the human skin in vitro and is readily absorbed by the gastrointestinal track. In view of the prevalence of phenols in different wastewaters and their toxicity to human and animal life even at low concentrations, it is extremely necessary to employ appropriate strategies for effective treatment of wastewater before discharging it into water bodies. (Anselmo and Novais, 1992; Koyama *et al.*, 1994; Mokrini *et al.*, 1997; Chan and Fu, 1998; Danis *et al.*, 1998; Reardon *et al.*, 2000; Backhaus *et al.*, 2001; Goncharuk *et al.*, 2002 and Ajay *et al.*, 2004).

46 These treatment methods for water purification involves the removal of undesirable chemical
47 compounds, biological contaminants, suspended solids and gases present in the contaminated
48 water (Ho *et al.*, 2009). Some of these treatment methods are adsorption, ion exchange,
49 reverse osmosis, chemical oxidation, precipitation, distillation, solvent extraction and bio-
50 remediation. Adsorption process has been established to be the most effective method for the
51 removal of colour, odour, organic and inorganic pollutants from wastewater (Krishnaiah *et*
52 *al.*, 2013) due to its ability to accumulate the gas or liquid solute on the surface of a solid or
53 liquid through formation of film of molecules or atoms called adsorbate (Goyal *et al.*, 2004).

54 Different adsorbents have been produced from different sources with the aim of removal of
55 phenol and other harmful contaminants from waste water. The degree of success recorded
56 from the use of commercially activated carbon in treatment of wastewater was encouraging.
57 However, it suffered two fundamental shortcomings such as; cost of activated carbon is
58 expensive and non-renewability of the substance. The shortcomings in the use of
59 commercially sourced activated carbon led to the use of other cheaper adsorbents. Djebbar *et*
60 *al.* (2012) investigated the possibility of using natural and activated clay as an adsorbent for
61 removal of phenol. The performance of the activated clay was better than natural clay but
62 cost of getting a natural clay was lower than activated one. Also, the comparison of
63 adsorption tendencies of both modified bentonitic clay and activated carbon was investigated
64 by Mostafa *et al* (2015). The adsorption capacity of activated carbon was greater than that
65 modified bentonite however, the adsorption of phenol using activated carbon decreased at pH
66 greater than 8.

67
68 The waste generated from agricultural by-products provided a cheaper alternative of
69 preparation of activated carbon. Some of these by-products used for activation carbon
70 production which are used primarily for removal of phenol and other harmful compounds in
71 waste water are corn cob, rice husk, coconut shell, palm shell, apple pulp, chickpea husk,
72 grain sorghum, pistachio nut shell, Shaddock peel, forest waste named *Lantana camara*, olive
73 mill waste and jute fiber (Diao *et al.*, 2002; Lua *et al.*, 2004; Senthilkumaar *et al.*, 2005; Tan
74 *et al.*, 2008; Hu *et al.*, 2009; Abdelkreem, 2013; Girish and Ramachandra, 2014; Bing *et*
75 *al.*, 2017 and Auwal *et al.*, 2018). Activated carbon produced from high carbon content
76 agricultural residues such as flamboyant pod bark, rice husk, soya beans hull, sugarcane
77 bagasse, peanut shell, and walnut shell possess good adsorbent properties which makes them
78 suitable for treatment of wastewater, adsorption of hazardous gases (Sugumaran *et al.*, 2012)
79 and fast adsorption kinetics which makes it applicable for treatment of high strength and low
80 volume organic wastewater (Tan *et al.*, 2008).

81 Flamboyant tree is a large, deciduous tree with fern-like leaves. The flamboyant pods are
82 pendulous, elongated, woody, compressed, up to 50 cm long and is considered as agricultural
83 waste, thereby creating a disposal problem. It composed largely of cellulose, hemicelluloses,
84 lignin, tannin and pectin. The adsorption properties of the flamboyant pod are enhanced by
85 the presence of lignocellulose in the chemical composition of flamboyant pods makes it to be
86 porous and fibrous (Sugumaran *et al.*, 2012). Also, participation of functional groups such as
87 hydroxyl, carboxyl and methoxyls in binding the solutes to its surface and enhanced its
88 adsorptive tendencies of over a wide range of pollutants.

89 The treatment of phenol and its derivatives in the effluents streams of chemical industries
90 wastewater using an agricultural waste for production of activated carbon as an adsorbent
91 will give an insight into the adsorptive behavior the activated carbon in the presence phenol is
92 the what this manuscript will be addressing. Also, the complex interactions among the

93 variables that affect adsorption and optimization of the variables for maximum removal of
94 phenol will be investigated with the aid a statistical tool Design Expert v. 6. 0.8.

95

96 **Materials and Method**

97 The materials used for preparation of activated carbon, steps used in production of activated
98 carbon, preparation of simulated wastewater, adsorption studies methods, kinetics of
99 adsorption and optimization studies will be described in this section of the manuscript.

100 **Materials and Wastewater Preparation**

101 The activated carbon used for this study was produced from flamboyant pod bark (FPBAC)
102 adopting the method published by Aremu *et al.*, 2017., 2,4,6-trichlorophenol (analytical
103 grade), distilled water, UV-Spectrophotometer (UV-6100A). All glassware used were
104 thoroughly washed with distilled water, and oven dried before use. 2,4,6-trichlorophenol
105 (analytical grade) was used for preparation of simulated waterwater. 50 mg/L of 2,4,6-
106 trichlorophenol was prepared by dissolving 50 mg of 2,4,6 trichlorophenol in 1L of distilled
107 water in standard volumetric flask. The procedure was repeated for preparation of 100, 150,
108 200 and 250 mg/L of 2,4,6-trichlorophenol (Alade *et al.*, 2012).

109 **Adsorption Studies**

110 Batch adsorption study was carried out to evaluate the adsorption performance of the
111 prepared adsorbent from the flamboyant bark pod. This was done by adding various dosage
112 of the prepared activated carbon (FPBAC) to 25 ml each of the prepared different initial
113 concentrations (50 mg/L, 100 mg/L, 150 mg/L, 200 mg/L and 250 mg/L) of 2,4,6-
114 trichlorophenol already prepared in 100 mL conical flasks. Adsorption was allowed to
115 proceed at three different agitation rates with the aid of rotary shaker (model). The contact
116 time was measured at 30 minutes interval for a total of 180 minutes. The effects of
117 temperature on the removal of 2,4,6-trichlorophenol (TCP) by FPBAC was investigated by
118 varying the temperature of the thermostat incubator shaker from 30 – 60 °C.. Samples were
119 taken at pre-set time intervals, filtered and the filtrate was analyzed for residue of 2,4,6-
120 trichlorophenol using UV-Spectrophotometer (UV-6100A) at wavelength of 296 nm.

121 The percentage removal of 2,4,6-trichlorophenol was evaluated using equation 1:

$$122 \quad \text{Removal (\%)} = \frac{C_o - C_f}{C_o} \quad 1$$

123 where, C_o and C_f are the liquid-phase 2,4,6-trichlorophenol concentrations at zero time and at
124 any time t , respectively.

125 The adsorption capacity of the adsorbent (FPB) was evaluated using equation 2:

$$126 \quad A_c = \frac{(C_o - C_f) V}{M} \quad 2$$

127 where,

128 A_c is the adsorptive capacity of the FPB, C_o (mg/L) is the initial concentration of 2,4,6-
129 trichlorophenol in contact with adsorbent, C_f (mg/L) is the final concentration of 2,4,6-
130 trichlorophenol after the batch adsorption procedure at any time t ,
131 M (g) is the mass of adsorbent used and V is the volume of the aqueous solution in liter (L).

132

133 **Design of Optimization Experiments**

134 The Central composite design (CCD) in the Design Expert software (6.0.2) was used to
135 evaluate the adsorption of 2,4,6-trichlorophenol on the produced activated carbon (FPBAC).
136 The dependent variable selected for this evaluation was adsorption capacity while the
137 independent variables were agitation, contact time, adsorbent dose and initial 2,4,6-
138 trichlorophenol concentration in wastewater. The range of the independent variables used for
139 CCD design and optimization studies are tabulated in table 1. Adsorption capacity was used
140 to determine the optimum conditions for the adsorption at an agitation, contact time,
141 adsorbent dosage and initial concentration. One-factor-at-a-time (OFAT) method was used to
142 study the effects of adsorption factors after obtaining the optimum conditions.

143

144 Table 1: Factors Level Selected for Adsorption Experiment

145

Factors	Units	Low (-1)	Mid (0)	High (+1)
Agitation	rpm	150	200	250
Contact time	min	60	90	120
Dosage	g	0.15	0.2	0.25
Initial conc.	mg/L	100	150	200

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147

148 **Results and Discussion**

149 The result of the CCD used for experimental studies of the adsorption capacity FPBAC
150 subject to four different parameters, one factor behavior, interaction influence, ANOVA and
151 model validation was presented in this section of the manuscript.

152 **Result of the Design**

153 The experimental runs for determination of adsorption capacity of flamboyant pod bark
154 activated carbon (FPBAC) as a function agitation, contact time, dosage and initial
155 concentration according to the design generated from CCD was tabulated in Table 2. A total
156 of thirty (30) experimental runs was generated.

157 It can be deduced from the table that adsorption factors (Agitation, contact time, adsorbent
158 dosage and initial concentration) has a significant effect on the adsorption capacity obtained.
159 Generally, it was found that adsorption capacity increase with increase agitation, contact time
160 and initial concentration of the adsorbate and decrease in adsorbent dosage. According to
161 Alam *et al.* (2007) an increase in agitation with contact time would enhance mass transfer of
162 the adsorbate to the surface of the adsorbents. The maximum adsorption capacity of 37.64
163 mg/g was obtained at run 2 at agitation of 200 rpm, contact time of 90 min, 0.10 g of
164 adsorbent dosage and 150 mg/L of initial concentration of the adsorbate while the minimum
165 adsorption capacity of 6.80 mg/g was obtained at run 21 at agitation of 200 rpm, contact time
166 of 90 min, 0.20 g of adsorbent dosage and 50 mg/L of initial concentration of the adsorbate.

167 The maximum adsorption capacity of 37.64 mg/g obtained for the material (FPB)
168 investigated in this study is well compared with 40 mg/g obtained from microporous ZnCl₂
169 activated coir pith carbon (Subha and Namasivayam, 2008) and well above 22.2 mg/g
170 obtained from activated carbon derived from oil palm empty fruit bunches (Alam *et al.*,
171 2007).

172 **Table 2. Central composite Design of Adsorption Experiment**

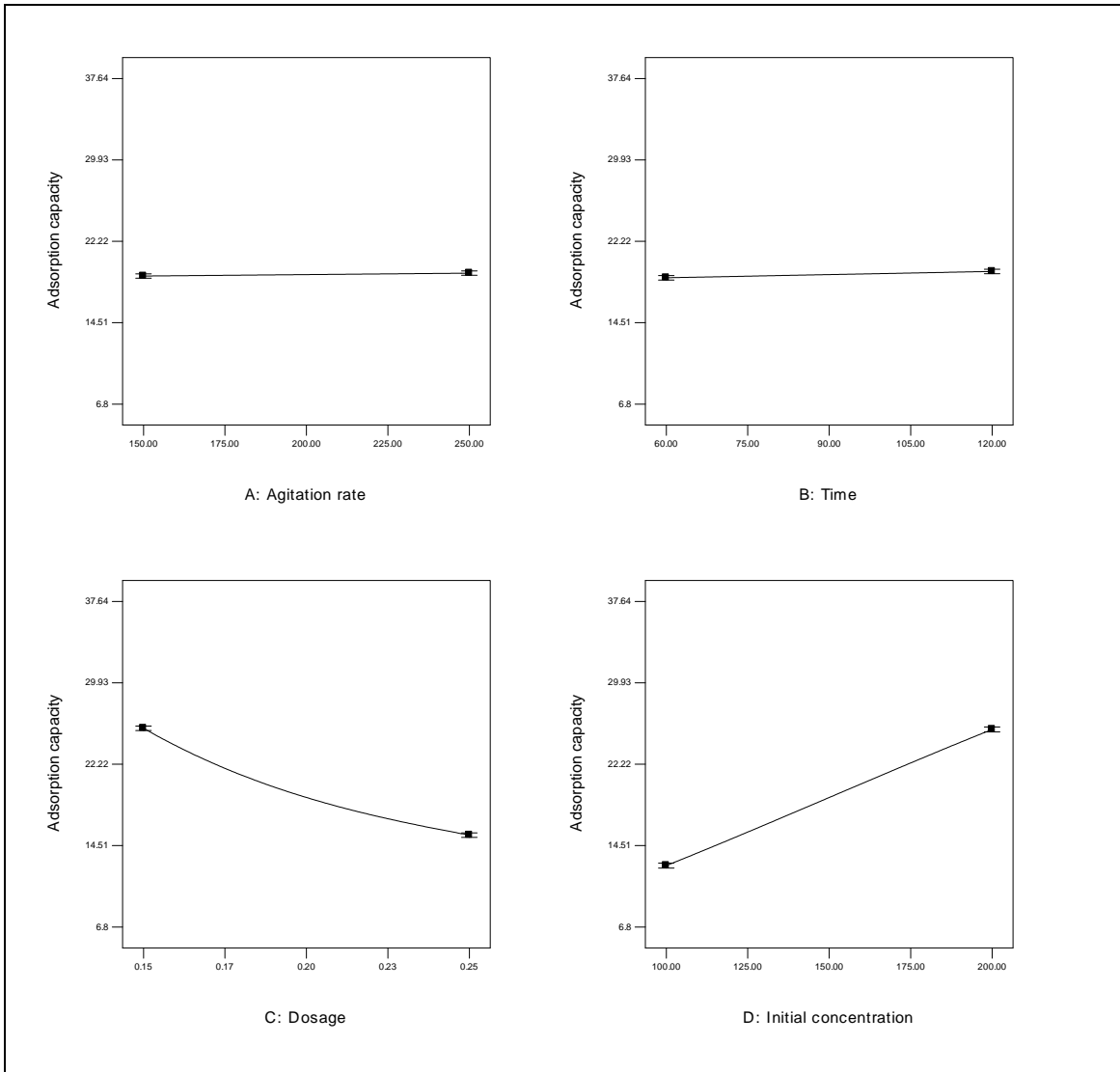
Run	Agitation rate (rpm)	Contact time(sec)	Dosage (g)	Initial concentration (mg/L)	Adsorption capacity (mg/g)
1	100	90	0.2	150	19.14
2	200	90	0.1	150	37.64
3	250	120	0.25	200	20.22
4	150	120	0.25	200	20.45
5	200	30	0.2	150	18.53
6	250	120	0.15	100	18.2
7	300	90	0.2	150	19.47
8	150	120	0.25	100	10.36
9	150	120	0.15	200	33.77
10	250	60	0.15	200	32.29
11	150	120	0.15	100	17.58
12	200	90	0.2	150	19.41
13	250	60	0.25	100	10.85
14	250	120	0.25	100	11.06
15	200	90	0.2	150	19.99
16	150	60	0.15	100	17.38
17	200	90	0.2	150	18.65
18	150	60	0.25	200	20.82
19	200	90	0.2	250	31.07
20	200	150	0.2	150	19.81
21	200	90	0.2	50	6.8
22	250	120	0.15	200	34.5
23	200	90	0.2	150	18.98
24	250	60	0.25	200	20.42
25	250	60	0.15	100	17.62
26	200	90	0.2	150	18.81
27	200	90	0.3	150	12.82
28	150	60	0.25	100	9.18
29	150	60	0.15	200	32.96
30	200	90	0.2	150	19.16

173

174 **One factor plot**

175 The behaviour of individual variables used for the modelling was presented in Figure 1. In
176 the figure, a variable was considered at a time while the other variables were fixed at the mid
177 points of the other variables. At constant values of 90 min, dosage of 0.2 g, and initial
178 concentration of 150 mg/L, the adsorptive capacity of slightly increased from 18.9 to 19.2
179 mg/g when agitation rate was increased from 150 to 250 rpm as shown in Figure 1(a). Similar
180 slight increase in adsorptive capacity from 18.77 to 19.37 mg/g was observed when contact
181 time of exposure was increased from 60 to 120 min as presented in Figure 1 (b). Increase in
182 adsorbent dosage from 0.15 to 0.25 cause a decrease in adsorption capacity from 25.6 to
183 15.51 mg/g at a constant values of agitation rate, contact time and initial concentration shown
184 in Figure 1 (c). The opposite of behaviour of adsorbent dosage on adsorptive capacity was

185 observed for initial concentration. The adsorptive capacity value increased from 12.62 to
 186 25.52 mg/g for an increase in initial concentration values ranging 100 to 200 mg/L.
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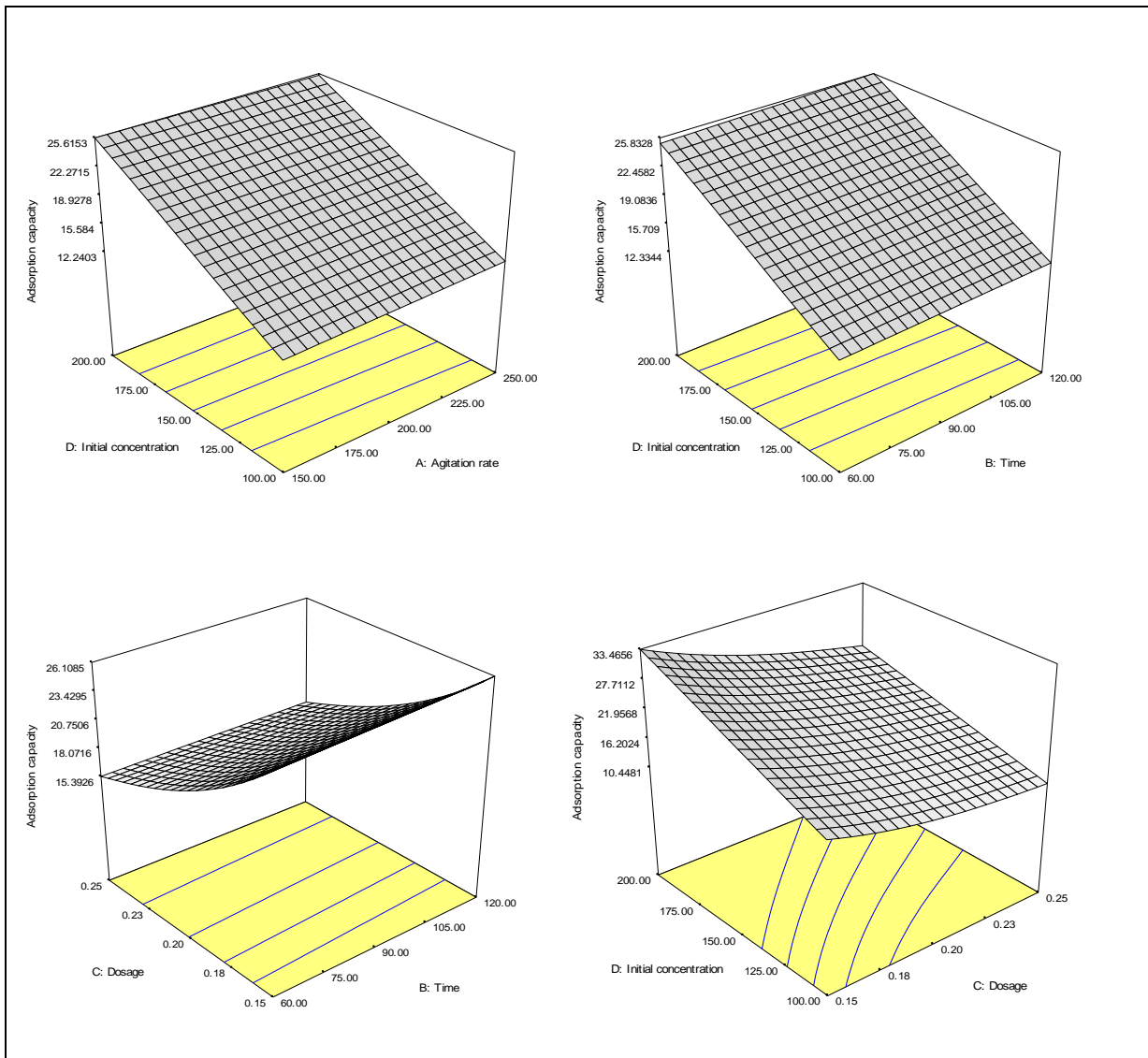


188 Figure 1. Influence of individual variables on adsorption capacity

189

190 **3D Surface Plot**

191 The combined effect of two variables and keeping the two remaining variables at midpoints
 192 was described in Figure 2. Figure 2 show the combined behaviour of agitation rate and initial
 193 concentration on the adsorptive capacity of the flamboyant pod adsorbent. At low Adsorbent
 194 dosage, adsorptive capacity slightly increased from 12.24 to 12.99 while at high adsorbent
 195 dosage, 200 g, the adsorptive capacity decreased from 25.6 to 25.41 for increase in agitation
 196 rate from 100 to 200 rpm. Increase in initial concentration from 100 to 200 mg/L caused an
 197 increase in adsorptive capacity from 12.24 to 25.6 and 12.99 to 25.41 at agitation rate of 100
 198 and 200 rpm respectively. Other combined 3D surface plots behaviour of the other variables.



201 Figure 2. 3D Surface plot of the variables used for model development

202

203 Model Fitting and Validation

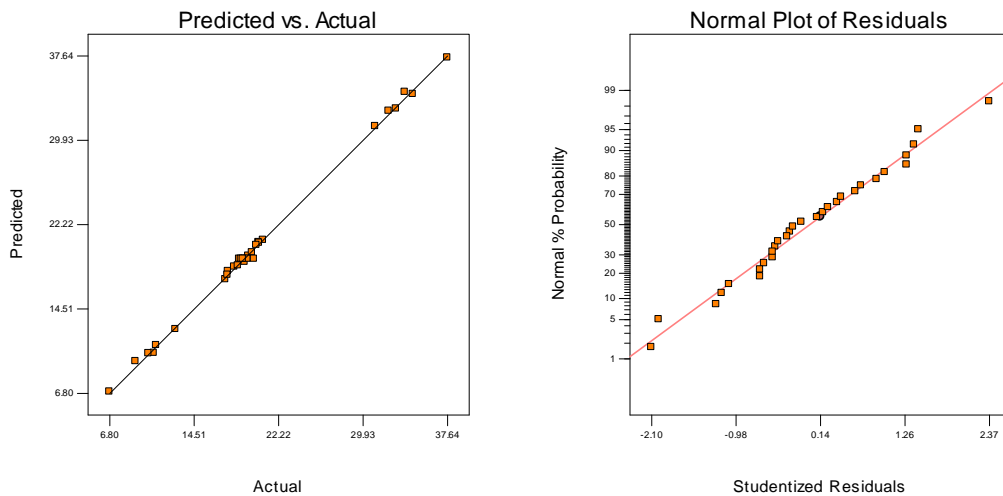
204 The regression model developed for the prediction of adsorptive capacity was a modified
 205 cubic polynomial model which was achieved through manual reduction of larger insignificant
 206 model terms in order to arrive at the empirical equation shown in equation 1. The
 207 coefficients of the model were obtained from multiple regression analysis as presented in
 208 Table 2. The coefficients preceding all the model terms with positive signs show synergistic
 209 effect, while the models with negative sign show antagonistic effect. The coefficients of
 210 model terms A, B, D, C^2 and BD positively affected adsorptive capacity model developed
 211 equation while C, AD, BC, CD, C^3 , D^3 and BCD negatively affect the adsorptive capacity
 212 model.

213 $A_c = 19.07 + 0.14 * A + 0.3 * B - 4.68 * C + 6.58 * D + 1.5 * C^2 - 0.24 * AD - 0.19 *$
 214 $BC + 0.018 * BD - 1.39 * CD - 0.38 * C^3 - 0.13 * D^3 - 0.26 * BCD$
 215 1.

216 **Model Validation**

217 The adsorptive capacity model developed was validated using residual and crossplot as
 218 shown in Fig. 3. Figure 3 show the response of the predicted values from the developed
 219 model was compared with the experimental values of adsorptive capacity of flamboyant pod.
 220 The correlation coefficient (r^2) and adjusted - r^2 values of the crossplot are 0.9985 and 0.9975,
 221 are close to 1 which show the model is a replica of the experimental result used in developing
 222 it. The other statistical parameter that support the accuracy of the model are adequate
 223 precision of 115.8 which show there was adequate signals for ease of navigation between the
 224 design space. The model was further analysed using a normal plot of the residuals. The test
 225 point residuals follow are within the 45° line on the plot. The graph show that no further
 226 improvement is required because the test points scattered and do not exhibit a ‘‘S-shaped’’
 227 curve.

228



229

230 Figure 3. The Crossplot and normal probability curve of the developed model

231 The analysis of variance (ANOVA) of the parameters used for model development are
 232 tabulated in Table 3. A probability value [(p model>F) < 0.05] show its highly significance
 233 to model equation while [(p model>F) > 0.05] show less or insignificant influence on the
 234 model equation. The following coded parameters B, C, D, C^2 , AD, CD, C^3 , D^3 , BCD are
 235 significant model terms. Values greater than 0.1000 indicate the model terms are not
 236 significant. The "Lack of Fit F value" of 0.56 showed that lack of fit is not a significant
 237 criterion to model developed with respect to pure error of 0.23. An 81.09 % chance of a
 238 "Lack of Fit F-value" of this magnitude could be because of noise.

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Table 3. ANOVA

Source	Sum of Squares	DF	Mean Square	F Value	Prob > F
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Model	1778.47	12	148.21	923.48	< 0.0001	significant
A	0.46	1	0.46	2.86	0.109	
B	2.15	1	2.15	13.38	0.0019	
C	174.97	1	174.97	1090.25	< 0.0001	
D	346.11	1	346.11	2156.62	< 0.0001	
C ²	64.64	1	64.64	402.8	< 0.0001	
AD	0.9	1	0.9	5.62	0.0298	
BC	0.56	1	0.56	3.46	0.0803	
BD	4.90E-03	1	4.90E-03	0.031	0.8634	
CD	31.02	1	31.02	193.32	< 0.0001	
C ³	7.01	1	7.01	43.66	< 0.0001	
D ³	0.78	1	0.78	4.86	0.0415	
BCD	1.1	1	1.1	6.87	0.0179	
Residual	2.73	17	0.16			
Lack of Fit						not significant
Pure Error	1.56	12	0.13	0.56	0.8109	
Cor	1.17	5	0.23			
Total	1781.2	29				

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Optimization Studies

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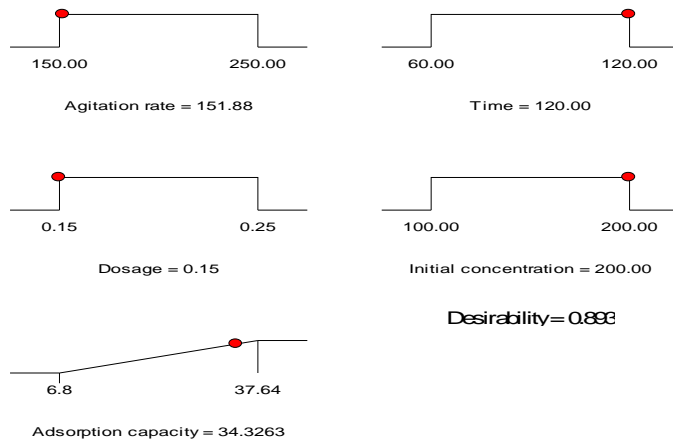
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The optimization analysis was conducted to determine the optimum conditions of all the four parameters that will maximize the adsorption capacity of FPBAC and analysed by desirability function of the dependent parameter (adsorption capacity). In the optimization analysis of numerical optimization in RSM, the adsorption capacity was maximized and the four process parameters agitation rate, contact time, dosage and initial concentration were all set within their range of values. The ramp of the numerical optimization in RSM for the adsorption capacity subject to the four parameters are shown in Figure 5. The maximum adsorption capacity of 34.33 was achieved when agitation rate, contact time, dosage and initial concentration were fixed at 151.88 rpm, 120 sec, 0.15 g and 200 mg/g given rise to a desirability of 0.893.



256

257 Figure 5. Ramp of the optimization study

258 Conclusion

259 The following deductions were reported from parametric study of influence of variables that
 260 affect the adsorptive capacity of FBPAC in removal of phenol from simulated wastewater:

- 261 ✓ The individual one-factor behaviour show that the initial concentration has the most
- 262 influential impact on the adsorptive capacity of FBPAC
- 263 ✓ The correlation coefficient (r^2) and adjusted r^2 recorded after validation of the model
- 264 was 0.9985 and 0.9975, are close to 1 which show the model is a replica of the
- 265 experimental result used in developing it.
- 266 ✓ The different behaviour exhibited for individual and interaction effects of variables
- 267 provided a basis for adjusting the values of the variables and such effect on adsorptive
- 268 capacity of FBPAC.
- 269 ✓ RSM was successfully used for the modelling of adsorption capacity of an adsorbent
- 270 produced from FBPAC in removing phenol in a simulated wastewater
- 271 ✓ The optimization studies placed the maximum adsorption capacity of FBPAC at 34.33
- 272 provided the agitation rate, contact time, dosage and initial concentration were fixed
- 273 at 151.88 rpm, 120 sec, 0.15 g and 200 mg/g respectively.

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